

638072 01
10740839

MOTION OF ELECTRON GAS IN CONDUCTING SOLIDS

By H. Demiray and A. C. Eringen

Technical Report No. 29

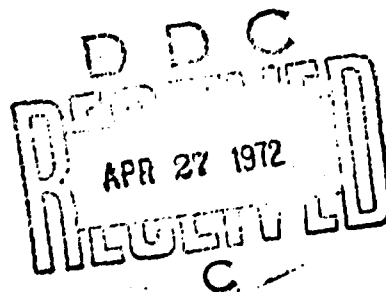
April, 1972

Office of Naval Research
Department of the Navy
Contract N-00014-67-A-0151-0004

PRINCETON UNIVERSITY
Department of Aerospace and Mechanical Sciences



Reproduced by
NATIONAL TECHNICAL
INFORMATION SERVICE
Springfield, Va 22151



Approved for public release; Distribution unlimited.

Unclassified

Security Classification

DOCUMENT CONTROL DATA - R & D

(Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified)

1. ORIGINATING ACTIVITY (Corporate author)		2a. REPORT SECURITY CLASSIFICATION Unclassified	
Princeton University		2b. GROUP	
3. REPORT TITLE Motion of Electron Gas in Conducting Solids			
4. DESCRIPTIVE NOTES (Type of report and inclusive dates) Research Report			
5. AUTHOR(S) (First name, middle initial, last name) Rilmi Demiray and A. Cemal Eringen			
6. REPORT DATE April, 1972		7a. TOTAL NO. OF PAGES 32	7b. NO. OF REFS 6
8a. CONTRACT OR GRANT NO. N-00014-67-A-0151-0004		8b. ORIGINATOR'S REPORT NUMBER(S) Technical Report #29	
b. PROJECT NO. N 064-410		9b. OTHER REPORT NO(S) (Any other numbers that may be assigned this report)	
10. DISTRIBUTION STATEMENT This document has been approved for public release and sale; its distribution is unlimited.			
11. SUPPLEMENTARY NOTES		12. SPONSORING MILITARY ACTIVITY Office of Naval Research Arlington, Virginia 22217	
13. ABSTRACT By use of the continuum theory of mixtures, a theory is presented for elastic conductors. The ionic lattice and electronic gas as separate continua constitute the members of the mixture. Balance laws and jump conditions are given, and a set of properly invariant constitutive equations are obtained and linearized. The field equations are solved for a problem of electrostatic probe, namely, a charged spherical cavity in a solid plasma.			

DD FORM 1473

(PAGE 1)

S/N 0101-807-6801

Unclassified

Security Classification

JND PFSO 13152

14

KEY WORDS

conducting elastic solids

charged solids

solid plasma

spherical cavity

electrostatic probe

LINK A

LINK B

LINK C

ROLE

WT

ROLE

WT

ROLE

WT

AMS Report No. 1037

MOTION OF ELECTRON GAS IN CONDUCTING SOLIDS

H. Demiray and A. C. Eringen

Department of Aerospace and Mechanical Sciences
Princeton University

Technical Report No. 29

April, 1972

to

Office of Naval Research

Department of the Navy

Contract N-00014-67-A-0151-0004

Project No. NR 064-410

Project Director:

A. C. Eringen

Approved for public release; Distribution unlimited.

MOTION OF ELECTRON GAS IN CONDUCTING SOLIDS*

H. Demiray and A. C. Eringen

Department of Aerospace and Mechanical Sciences

Princeton University

Princeton, New Jersey 08540

ABSTRACT

By use of the continuum theory of mixtures, a theory is presented for elastic conductors. The ionic lattice and electronic gas as separate continua constitute the members of the mixture. Balance laws and jump conditions are given, and a set of properly invariant constitutive equations are obtained and linearized. The field equations are solved for a problem of electrostatic probe, namely, a charged spherical cavity in a solid plasma.

* This work was supported by the Office of Naval Research.

1. INTRODUCTION

In recent years, a revival of interest has reopened research in the field of electromagnetic elastic solids. Besides growing technological importance, certain fundamental questions hitherto unresolved gave impetus to these studies. Among them are the nature of electromagnetic force, energy, and the question of invariance of the constitutive functions. In continuum theories, Euclidean invariance and the principle of objectivity are taken as fundamental, while in electromagnetic theory, the Lorentz invariance is basic. For deformable bodies subject to electromagnetic fields, a unification and reconciliation of these two points of view was necessary (cf. Grot and Eringen [1], Jordan and Eringen [2], and Walker [3]). In these works, a continuum was assumed to possess no electron inertia, so that the electromagnetic force on the current was transmitted directly to the solid continuum. In reality, in fact, the force acting on the current is transmitted to a solid continuum through momentum transferred by the electrons.

In a recent work [4], we presented a continuum theory of charged mixtures capable of diffusion, ionization, and recombination. In this work, the effect of the diamagnetic property of electrons and ions was also included. Here we consider a mixture composed of polarizable and magnetizable conductors and an electron gas continuum that possesses inertia.

Theory developed here is believed to have potential application in the discussion of electrical charges in solids in particular in lightning damage, although the latter problem requires the inclusion of thermal effects, in the discussion of near fields.

2. BALANCE EQUATIONS

The balance equations of a mixture composed of an elastic conductor and an electron gas continuum may be obtained as a special case of equations (2.1) to (4.6) of reference [4], with the constraints that

$$(2.1) \quad C_{(\alpha)} = 0, \quad \Lambda_{(\alpha)} = 0, \quad \alpha = e, s$$

$$P_{(\alpha)} = 0, \quad M_{(\alpha)} = 0, \quad \alpha = e$$

where $C_{(\alpha)}$ and $\Lambda_{(\alpha)}$ are respectively the mass production (or destruction) and the rate of polarization transfer, $P_{(\alpha)}$ is the partial polarization, and $M_{(\alpha)}$ is the partial magnetization of species α which takes the values s and e associating the fields, respectively, with the ionic lattice and electronic gas continua. The balance laws and jump conditions are:

(i) Conservation of Mass:

$$(2.2) \quad \frac{\partial \rho_{(\alpha)}}{\partial t} + \text{div}(\rho_{(\alpha)} \underline{v}_{(\alpha)}) = 0 \quad \text{in } V_{(\alpha)} - \sigma$$

$$(2.3) \quad [\rho_{(\alpha)} (\underline{v}_{(\alpha)} - \underline{u})] \cdot \underline{n} = 0 \quad \text{on } \sigma$$

where $\rho_{(\alpha)}$, $\underline{v}_{(\alpha)}$ are respectively the density and the velocity of the α th species, and \underline{u} is the velocity of a moving discontinuity surface σ with exterior normal \underline{n} .

(ii) Balance of Momentum:

$$(2.4) \quad t_{(\alpha);k}^{kl} + g_{(\alpha)}^l + \rho_{(\alpha)} (f_{(\alpha)}^l - \hat{v}_{(\alpha)}^l) = R_{(\alpha)}^l \quad \text{in } V_{(\alpha)} - \sigma$$

$$(2.5) \quad [\rho_{(\alpha)} (\underline{v}_{(\alpha)}^k - \underline{u}^k) \underline{v}_{(\alpha)}^l - t_{(\alpha)}^{kl}] n_k = \hat{R}_{(\alpha)}^l \quad \text{on } \sigma$$

with $R_{(\alpha)}^k$ and $\hat{R}_{(\alpha)}^k$ subject to

$$(2.6) \quad \sum_{\alpha} R_{(\alpha)}^k = 0, \quad \sum_{\alpha} \hat{R}_{(\alpha)}^k = 0$$

where $t_{(\alpha)}$, $f_{(\alpha)}$, $R_{(\alpha)}$, $\hat{R}_{(\alpha)}$ and $g_{(\alpha)}$ are, respectively, the stress tensor, mechanical body force, the linear momentum transfer in volume $V_{(\alpha)} - \sigma$ and on the surface σ , and the body force due to electromagnetic origin defined by

$$(2.7) \quad \begin{aligned} g_i^{(s)} &\equiv q_{(s)} E_i^{(s)} + E_{i;m}^{(s)} p_m^{(s)} + \epsilon_{ijk} p_j^{*(s)} B^k + M_k^{(s)} B_{;i}^k \\ g_i^{(e)} &\equiv q_{(e)} E_i^{(e)} \end{aligned}$$

Here $q_{(\alpha)}$, $E_{(\alpha)}$, B , $M_{(\alpha)}$, $P_{(\alpha)}$ and $\dot{P}_{(\alpha)}^*$ are respectively the charge density, effective electric field, magnetic field, magnetization, polarization, and the convective time rate of polarization defined by

$$(2.8) \quad \begin{aligned} E_{(\alpha)} &\equiv E + \frac{v_{(\alpha)}}{c} \times B \\ \dot{P}_{(\alpha)}^i &\equiv \dot{P}_{(\alpha)}^i + P_{(\alpha)}^i v_{(\alpha)r}^r - P_{(\alpha)}^j v_{(\alpha);j}^j \end{aligned}$$

Throughout this work, a semi-colon is used to indicate the covariant partial differentiation and a superposed prime the material derivative of tensor fields following the motion of the α th species.

(iii) Balance of Moment of Momentum:

$$(2.9) \quad t_{(\alpha)}^{kl} - t_{(\alpha)}^{lk} + \epsilon^{klm} (G_m^{(\alpha)} + T_m^{(\alpha)}) = 0 \quad \text{in } V_{(\alpha)} - \sigma$$

$$(2.10) \quad \hat{T}_{(\alpha)}^k = 0 \quad \text{on } \sigma$$

with $T_{(\alpha)}^k$ and $\hat{T}_{(\alpha)}^k$ subject to

$$(2.11) \quad \sum_{\alpha} T_{(\alpha)}^k = 0, \quad \sum_{\alpha} \hat{T}_{(\alpha)}^k = 0$$

where $T_{(\alpha)}$, $\hat{T}_{(\alpha)}$, and $G_{(\alpha)}^k$ are respectively the rates of angular momentum transfer in volume $V_{(\alpha)} - \sigma$ and on the surface σ , and the electromagnetic couple defined by

$$(2.12) \quad G_{(s)} \equiv P_{(s)} \times E_{(s)} + M_{(s)} \times B, \quad G_{(e)} \equiv 0$$

(iv) Conservation of Energy:

$$(2.13) \quad \rho_{(s)} \epsilon'_{(s)} = t_{(s)}^{kl} v_{l;k}^{(s)} + \rho_{(s)} E_1^{(s)} \left(\frac{P_1^{(s)}}{(s)} \right)' - M_{(s)}^i B_1^i + \frac{1}{2\theta_{(s)}} R_{(e)}^l u_l^{(es)} + q_{(s);k}^k + \rho_{(s)} h_{(s)} + e_{(s)}$$

$$(2.14) \quad \rho_{(e)} \epsilon'_{(e)} = t_{(e)}^{kl} v_{l;k}^{(e)} + \frac{1}{2\theta_{(e)}} R_{(e)}^l u_l^{(es)} + q_{(e);k}^k + \rho_{(e)} h_{(e)} + e_{(e)}$$

$$(2.15) \quad \left[\rho_{(\alpha)} (\epsilon_{(\alpha)} + \frac{1}{2} v_{(\alpha)}^2) (v_{(\alpha)}^k - u^k) - t_{(\alpha)}^{kl} v_l^{(\alpha)} - q_{(\alpha)}^k \right] n_k = \hat{e}_{(\alpha)}, \text{ on } \sigma$$

where $e_{(\alpha)}$ and $\hat{e}_{(\alpha)}$ are subject to

$$(2.16) \quad \sum_{\alpha} e_{(\alpha)} = 0, \quad \sum_{\alpha} \hat{e}_{(\alpha)} = 0$$

Here $\epsilon_{(\alpha)}$, $h_{(\alpha)}$, $q_{(e)}$, $e_{(\alpha)}$ and $\hat{e}_{(\alpha)}$ are respectively the internal energy density, volume heat supply, surface heat flux, and the values of the rate of energy transfer in volume $V_{(\alpha)} - \sigma$ and on the surface σ of the α th component.

(v) Principle of Entropy:

$$(2.17) \quad \rho_{(\alpha)} \eta'_{(\alpha)} - \left(\frac{q_{(\alpha)}^k}{\theta_{(\alpha)}} \right)_{;k} - \frac{\rho_{(\alpha)} h_{(\alpha)}}{\theta_{(\alpha)}} + n_{(\alpha)} \geq 0, \text{ in } V_{(\alpha)} - \sigma$$

$$(2.18) \quad [\rho_{(\alpha)} \eta_{(\alpha)} (v_{(\alpha)}^k - u^k) - \frac{q_{(\alpha)}^k}{\theta_{(\alpha)}}] n^k + \hat{n}_{(\alpha)} \geq 0 \text{ on } \sigma$$

where $n_{(\alpha)}$ and $\hat{n}_{(\alpha)}$ are subject to

$$(2.19) \quad \sum_{\alpha} n_{(\alpha)} \geq 0, \quad \sum_{\alpha} \hat{n}_{(\alpha)} = 0$$

Here $\eta_{(\alpha)}$, $n_{(\alpha)}$ and $\hat{n}_{(\alpha)}$ are respectively the entropy volume density and the rate of entropy transfer in volume $V_{(\alpha)} - \sigma$ and on the surface σ of the α th component.

For convenience we introduce the following Legendre transformation

$$(2.20) \quad \begin{aligned} \psi_{(s)} &\equiv \varepsilon_{(s)} - \theta_{(s)} \eta_{(s)} + \frac{M_{(s)} \cdot B}{\rho_{(s)}} \\ \psi_{(e)} &\equiv \varepsilon_{(e)} - \vartheta_{(e)} \eta_{(e)} \end{aligned}$$

Carrying (2.20) into (2.17) and eliminating the $\rho_{(\alpha)} h_{(\alpha)}$ from (2.17), by use of (2.13) and (2.14), we obtain a new form for the energy inequality

$$(2.21) \quad - \frac{\rho_{(s)}}{\theta_{(s)}} (\eta_{(s)} \theta'_{(s)} + \dot{\psi}_{(s)}) + \frac{1}{\theta_{(s)}} t_{(s)}^{kl} v_{l;k}^{(s)} + \frac{1}{\theta_{(s)}} E_{(s)}^i \dot{p}_i^{(s)} + \frac{1}{\theta_{(s)}} B_{(s)}^{i1} \dot{M}_i^{(s)} \\ + \frac{1}{2\theta_{(s)}} R_{(e)}^l u_l^{(es)} + \frac{q_{(s)}^k \theta_{(s)}}{\theta_{(s)}^2}{}_{;k} + \frac{e_{(s)}}{\theta_{(s)}} + n_{(s)} \geq 0$$

$$(2.22) \quad - \frac{\rho_{(e)}}{\theta_{(e)}} (\eta_{(e)} \theta'_{(e)} + \dot{\psi}_{(e)}) + \frac{1}{\theta_{(e)}} t_{(e)}^{kl} v_{l;k}^{(e)} + \frac{1}{2\theta_{(e)}} R_{(e)}^l u_l^{(es)} \\ + \frac{q_{(e)}^k \vartheta_{(e)}}{\theta_{(e)}^2}{}_{;k} + \frac{e_{(e)}}{\theta_{(e)}} + n_{(e)} \geq 0$$

Here $\bar{t}_{(s)}^{kl}$ is defined by

$$(2.23) \quad \bar{t}_{(s)}^{kl} \equiv t_{(s)}^{kl} + (P_{(s)} \cdot E^{(s)} + M_{(s)} \cdot B) g^{kl}$$

where g^{kl} is the metric tensor of the spatial frame of reference x .

These inequalities must be valid for all independent processes.

(vi) Electromagnetic Field Equations:

$$(2.24) \quad \nabla \times \underline{E} + \frac{1}{c} \frac{\partial \underline{B}}{\partial t} = 0, \quad [\underline{E}] \times \underline{n} + \frac{1}{c} [\underline{B}] \underline{u} \cdot \underline{n} = 0$$

$$(2.25) \quad \nabla \times \underline{H} = \frac{1}{c} \frac{\partial \underline{D}}{\partial t} + \frac{4\pi}{c} \underline{J}, \quad [\underline{H}] \times \underline{n} = \frac{1}{c} [\underline{D}] \underline{u} \cdot \underline{n} + \frac{4\pi}{c} \underline{\hat{J}}$$

$$(2.26) \quad \nabla \cdot \underline{D} = 4\pi q, \quad [\underline{D}] \cdot \underline{n} = 4\pi \hat{q}$$

$$(2.27) \quad \nabla \cdot \underline{B} = 0, \quad [\underline{B}] \cdot \underline{n} = 0$$

where \underline{E} , \underline{D} , \underline{H} , \underline{B} , \underline{J} , q , $\underline{\hat{J}}$ and \hat{q} are respectively the electric field, electric displacement, magnetic field, magnetic induction, and the values of the current and charge in volume $V-\sigma$ and on the surface of discontinuity σ .

These quantities are related to each other by

$$(2.28) \quad \begin{aligned} \underline{D} &\equiv \underline{E} + 4\pi \underline{P}_{(s)}, \quad \underline{H} \equiv \underline{B} - 4\pi (\underline{M}_{(s)} + \frac{\underline{v}_{(s)}}{c} \times \underline{P}_{(s)}) \\ \underline{\hat{J}} &\equiv q_{(s)} \underline{v}_{(s)} + q_{(e)} \underline{v}_{(e)} \\ q &\equiv q_{(s)} + q_{(e)} \end{aligned}$$

3. CONSTITUTIVE EQUATIONS

We select velocity, magnetization, and polarization of a solid as well as the density of electron gas and the first gradient of deformation of an elastic solid continuum as independent constitutive variables, i.e.,

$$(3.1) \quad v_{(\beta)}^k, P_{(s)}^k, M_{(s)}^k, \frac{\partial x^k}{\partial X_{(s)}^K} \equiv x_{,K}^k, \rho_{(e)}, \theta_{(\beta)}$$

The dependent variables are:

$$(3.2) \quad t_{(\alpha)}^{kl}, \psi_{(\alpha)}, n_{(\alpha)}, q_{(\alpha)}^k, R_{(\alpha)}^k, \dot{E}_{(s)}^k, B^k, e_{(\alpha)}, n_{(\alpha)}$$

The constitutive equations that obey the principle of equipresence have the following functional forms,

$$(3.3) \quad t_{(\alpha)}^{kl} = t_{(\alpha)}^{kl}(\rho_{(e)}, \theta_{(\beta)}, u_{(es)}^i, P_{(s)}^k, M_{(s)}^k, x_{,K}^k)$$

similar forms being valid for other constitutive variables.

The local Clausius-Duhem inequality imposes the following restrictions on the free energies

$$(3.4) \quad \begin{aligned} \psi_{(s)} &= \psi_{(s)}(\theta_{(s)}, P_{(s)}^k, M_{(s)}^k, x_{,K}^k) \\ \psi_{(e)} &= \psi_{(e)}(\theta_{(e)}, \rho_{(e)}) \end{aligned}$$

Substitution of (3.4) into (2.21) and (2.22) yields

$$\begin{aligned}
 & - \frac{\rho(s)}{\theta(s)} (\eta(s) + \frac{\partial \psi(s)}{\partial \theta(s)} \theta(s) + \frac{1}{\theta(s)} (t_{;s}^{kl} - \rho(s) \frac{\partial \psi(s)}{\partial x_{l,K}} x_{;K}^k) v_{l;k}^{(s)} \\
 (3.5) \quad & + \frac{1}{\theta(s)} (\xi_{;s}^i - \rho(s) \frac{\partial \psi(s)}{\partial p_i(s)} p_i(s) + \frac{1}{\theta(s)} (B^i - \rho(s) \frac{\partial \psi(s)}{\partial M_i(s)} M_i(s) \\
 & + \frac{1}{2\theta(s)} R_{(e)}^l u_l^{(es)} + \frac{q(s)}{\theta(s)} \theta_{;k}^k + \frac{e(s)}{\theta(s)} : n(s) \geq 0
 \end{aligned}$$

A similar form may be given for the electron continuum.

Further simplification of (3.5) can be accomplished if we note that $v_{l;k}^{(a)}$, $p_i^{(s)}$, $M_i^{(s)}$ and $\theta_{;k}^{(a)}$ may be varied arbitrarily. The necessary and sufficient conditions for the inequality (3.5) to be valid for all arbitrary variations of these quantities is that the coefficients of these quantities must vanish, i.e.,

$$(3.6) \quad \eta_{(a)} = - \frac{\partial \psi(a)}{\partial \theta(a)} \quad , \quad q_{(a)}^k = 0 \quad , \quad a = e, s$$

$$\begin{aligned}
 (3.7) \quad & t_{(e)}^{kl} = - \rho_{(e)}^2 \frac{\partial \psi(e)}{\partial p_{(e)}} \delta^{kl} \\
 & t_{(s)}^{kl} = \rho(s) \frac{\partial \psi(s)}{\partial x_{l,K}} x_{;K}^k - (P_{(s)} \cdot E^{(s)} + M_{(s)} \cdot B) \delta^{kl} \\
 (3.8) \quad & E_{(s)}^k = \rho(s) \frac{\partial \psi(s)}{\partial p_k(s)} \quad , \quad B^k = \rho(s) \frac{\partial \psi(s)}{\partial M_k(s)}
 \end{aligned}$$

subject to

$$(3.9) \quad \epsilon_{klm} \left(\frac{\partial \psi(s)}{\partial p_k(s)} p_{(s)}^l + \frac{\partial \psi(s)}{\partial M_k(s)} M_{(s)}^l + \frac{\partial \psi(s)}{\partial x_{k,K}} x_{;K}^l \right) = 0$$

At this point, a remark is in order: Since we are dealing with the dynamics of deformable electromechanical materials, then a question

arises as to whether the free energy density is invariant under transformations of the spatial frame of reference or not. Clearly, it is not unless one replaces $P_{(s)}^k$ and $M_{(s)}^k$ by $P_{(s)}^k$ and $M_{(s)}^k$, where $P_{(s)}^k$ and $M_{(s)}^k$ are respectively the values of polarization and magnetization measured on the coordinate frame moving with material body. However, the energy equation is written in terms of $P_{(s)}^k$ and $M_{(s)}^k$, therefore, such a replacement is not suitable because of the restrictions imposed by the second law of thermodynamics. Another way of handling this difficulty is to introduce a fictitious rate of electromagnetic momentum so as to obtain an energy equation written in terms of $P_{(s)}^k$ and $M_{(s)}^k$. The electromagnetic momentum so introduced is not unique and requires modification of Cauchy's law, thus opening new questions.

As a result, the question of invariance requirements for deformable bodies subject to electromagnetic fields is still an open question and must be studied separately. In this regard, we refer the readers to works by Dixon and Eringen [5] and Toupin [6] who eventually used similar formulations that we employ here. The present formulation is certainly applicable for cases where the component of the magnetic flux perpendicular to the particle velocity is very small as compared to the component parallel to the particle velocity.

Carrying (3.6) to (3.9) into (3.5), the inequalities (3.5) are simplified to

$$(3.10) \quad \frac{1}{2\theta_{(e)}} R_{(e)}^l u_l^{(es)} + \frac{e_{(e)}}{\theta_{(e)}} + n_{(e)} \geq 0$$

$$(3.11) \quad \frac{1}{2\theta_{(s)}} R_{(s)}^l u_l^{(es)} + \frac{e_{(s)}}{\theta_{(s)}} + n_{(s)} \geq 0$$

The principle of objectivity requires that $\Psi_{(s)}$ must have the following form

$$(3.12) \quad \Psi_{(s)} = \Psi_{(s)}(\theta^{(s)}, E_{KL}, P_K, M_K)$$

where E_{KL} , P_K , and M_K are defined by

$$(3.13) \quad 2 E_{KL} = g_{kl} x^k_{,K} x^l_{,L} - G_{KL}$$

$$P_K = g_{kl} x^k_{,K} P^l, \quad M_K = g_{kl} x^k_{,K} M^l$$

Here E_{KL} is the Lagrangian strain tensor defined on the material coordinate system X^K whose metric tensor is G_{KL} . The constitutive equations for the stress tensor, electric field, and magnetic flux now take the forms

$$(3.14) \quad t^{kl}_{(s)} = \rho_{(s)} \frac{\partial \Psi_{(s)}}{\partial E_{KL}} x^k_{,K} x^l_{,L} + E^k_{(s)} P^l_{(s)} + B^k M^l_{(s)} - (P_{(s)} \cdot E_{(s)} + M_{(s)} \cdot B) g^{kl}$$

$$(3.15) \quad E^k_{(s)} = \rho_{(s)} \frac{\partial \Psi_{(s)}}{\partial P_K} x^k_{,K}, \quad B^k = \rho_{(s)} \frac{\partial \Psi_{(s)}}{\partial M_K} x^k_{,K}$$

Here, it is seen from (3.14) that the condition (2.9) is satisfied if

$$(3.16) \quad T^k_{(a)} = 0, \quad a = e, s$$

From this general formulation, various order constitutive equations may be obtained. In particular for isotropic materials, the stress tensor, electric and magnetic fields can be expressed in terms of certain invariants

of independent state variables. Such a case has been given by Grot and Eringen [1] for a single medium, therefore we do not repeat them here. In what follows we will be interested in the linear constitutive equations.

4. LINEAR CONSTITUTIVE EQUATIONS

For the linear constitutive theory, the difference between material and spatial coordinates may be disregarded. In this case, the constitutive equations presented in (3.14) to (3.15) reduce to

$$(4.1) \quad t_{(s)}^{kl} = \rho_{(s)} \frac{\partial \psi(s)}{\partial e_{kl}} + E_{(s)}^k p_{(s)}^l + B_{(s)}^{kl} M_{(s)} - (p_{(s)} E_{(s)} + M_{(s)} B) g^{kl}$$

$$(4.2) \quad E_{(s)}^k = \rho_{(s)} \frac{\partial \psi(s)}{\partial p_k}, \quad B^k = \rho_{(s)} \frac{\partial \psi(s)}{\partial M_k}$$

Here, the infinitesimal strain tensor e^{kl} is defined by

$$(4.3) \quad e_{kl} \equiv \frac{1}{2} (u_{k;l} + u_{l;k})$$

where u is the displacement vector.

For linearly isotropic materials, we express the free energy of solid continuum as

$$(4.4) \quad \psi(s) = \frac{1}{2\rho_0(s)} (e_r^r)^2 + \frac{\mu}{\rho_0(s)} e^{kl} e_{kl} + \frac{\chi_1}{2\rho(s)} p_{(s)}^2 + \frac{\chi_2}{2\rho(s)} M_{(s)}^2$$

where λ , μ , χ_1 , χ_2 are the material constants, and $\rho_0(s)$ and $\rho(s)$ are, respectively the mass density in the undeformed and deformed bodies. The

$$(4.5) \quad \rho(s) = \rho_0(s) (1 - e_r^r)$$

Inserting (4.4) into (4.1) and (4.2), and using (4.5), the linear constitutive equations are obtained to be

$$(4.6) \quad E_{(s)}^k = \chi_1 p_{(s)}^k, \quad B^k = \chi_2 M_{(s)}^k$$

$$(4.7) \quad \begin{aligned} t_{(s)}^{kl} = & \lambda e_r^r g^{kl} + 2\mu e^{kl} + E_{(s)}^k P_{(s)}^l + v^k M_{(s)}^l \\ & - \frac{1}{2} (P_{(s)} \cdot E_{(s)} + M_{(s)} \cdot B) g^{kl} \end{aligned}$$

Here we have neglected the powers of infinitesimal strain tensor higher than the first.

In equation (4.7) it is interesting to note that the total stress tensor $t_{(s)}^{kl}$ of solid continuum consists of two parts: The first part is the classical Hook's law, and the second part is none other than Maxwell stress tensor.

In the linear theory, the forms of the rate of linear momentum transfer, energy and entropy transfers are (cf. [4])

$$(4.8) \quad R_{(e)}^k = v u_{(es)}^k - \tau P_{(s)}^k$$

$$(4.9) \quad \begin{aligned} e_{(e)} = & \beta_0 (\theta_{(s)} - \theta_{(e)}) + \beta_1 u_{(es)}^2 + \beta_2 e_r^r + \beta_3 (e_r^r)^2 \\ & + \beta_4 e^{kl} e_{kl} + \beta_5 M_{(s)}^2 + \beta_6 P_{(s)}^2 + \beta_7 u_{(es)} \cdot P_{(s)} \end{aligned}$$

$$(4.10) \quad \begin{aligned} n_{(e)} = & - \frac{\beta_0 (\theta_{(s)} - \theta_{(e)})}{\theta} + \gamma_1 u_{(es)}^2 + \gamma_2 e_r^r + \gamma_3 (e_r^r)^2 \\ & + \gamma_4 e^{kl} e_{kl} + \gamma_5 M_{(s)}^2 + \gamma_6 P_{(s)}^2 + \gamma_7 u_{(es)} \cdot P_{(s)} \end{aligned}$$

Material moduli v , τ , β_0 to β_7 and γ_1 to γ_7 appearing in (4.8) to (4.10) are functions of density of electron continuum.

The local Clausius-Duhem inequality imposes the following restrictions on these coefficients

$$\begin{aligned}
 \beta_0 &\geq 0 ; \frac{1}{2} v \mp \left(\frac{\theta(e)}{\theta(s)} \right) \gamma_1 \mp \beta_1 \geq 0 ; \mp \beta_6 \mp \left(\frac{\theta(e)}{\theta(s)} \right) \gamma_6 \geq 0 \\
 \left(\frac{1}{2} v \mp \beta_1 \mp \left(\frac{\theta(e)}{\theta(s)} \right) \gamma_1 \right) \left(\mp \beta_6 \mp \left(\frac{\theta(e)}{\theta(s)} \right) \gamma_6 \right) - \frac{1}{4} \left(\tau \mp \beta_7 \mp \left(\frac{\theta(e)}{\theta(s)} \right) \gamma_7 \right)^2 &\geq 0 \\
 \mp \beta_2 \mp \left(\frac{\theta(e)}{\theta(s)} \right) \gamma_2 &= 0 , \mp \beta_3 \mp \left(\frac{\theta(e)}{\theta(s)} \right) \gamma_3 \geq 0 , \mp \beta_4 \mp \left(\frac{\theta(e)}{\theta(s)} \right) \gamma_4 \geq 0 \\
 (4.11) \quad \mp \beta_5 \mp \left(\frac{\theta(e)}{\theta(s)} \right) \gamma_5 &\geq 0
 \end{aligned}$$

where it is understood that plus sign is for the solid continuum and the minus sign for the electrons.

The field equations from (2.2) to (2.28), with constant and equal temperatures, are given by

$$(4.12) \quad \frac{\partial \rho(e)}{\partial t} + \text{div} (\rho(e) \underline{v}(e)) = 0$$

$$(4.13) \quad -\nabla \pi(e) + q(e) \underline{E}(e) + \rho(e) \left(\underline{f}(e) - \underline{v}(e) \right) = v \underline{u}(e) - \tau \underline{P}(s)$$

$$(4.14) \quad \frac{\partial \rho(s)}{\partial t} + \text{div} (\rho(s) \underline{v}(s)) = 0$$

$$\begin{aligned}
 (4.15) \quad &(\lambda + \mu) \nabla \nabla \cdot \underline{u} + \mu \nabla^2 \underline{u} + q(s) \underline{E}(s) + (\underline{P}^*(s) \times \underline{B}) \\
 &+ \nabla \cdot [2 \underline{P}(s) \otimes \underline{E}(s) + \underline{M}(s) \otimes \underline{B} - \frac{1}{2} \underline{P}(s) \cdot \underline{E}(s) \underline{g}] + \rho(s) \left(\underline{f}(s) - \underline{v}(s) \right) \\
 &= v \underline{u}(s) + \tau \underline{P}(s)
 \end{aligned}$$

where $q(s)$ and $\pi(e)$ are defined by

$$(4.16) \quad q(s) \equiv q(s) - \nabla \cdot \underline{P}(s) , \quad \pi(e) = \rho(e)^2 \frac{\partial \psi(e)}{\partial \rho(e)}$$

In addition, we have Maxwell's equations

$$(4.17) \quad \nabla \times \underline{E} + \frac{1}{c} \frac{\partial \underline{B}}{\partial t} = 0, \quad \nabla \times \underline{H} = \frac{1}{c} \frac{\partial \underline{D}}{\partial t} + \frac{4\pi}{c} \underline{J}$$

$$(4.18) \quad \nabla \cdot \underline{D} = 4\pi q, \quad \nabla \cdot \underline{B} = 0$$

where \underline{H} and \underline{D} are defined by

$$(4.19) \quad \underline{H} \equiv \underline{B} + 4\pi \left(\frac{\underline{v}(s)}{c} \underline{P}(s) - \underline{M}(s) \right), \quad \underline{D} \equiv \underline{E} + 4\pi \underline{P}(s)$$

These equations together with corresponding jump conditions may be used to determine the electromagnetic and mechanical fields completely.

5. EQUATIONS OF ELASTIC CONDUCTORS

To obtain a continuum theory of elastic conductors, we assume that the inertia and thermodynamic pressure of electronic continuum are small as compared to the inertia and stress of elastic continuum. Under these assumptions, by summing equations (4.13) and (4.15) and neglecting the electron inertia and pressure, we obtain the field equations of elastic conductors

$$(5.1) \quad (\lambda + \mu) \nabla \nabla \cdot \underline{u} + \mu \nabla^2 \underline{u} + q^t \underline{E} + \underline{P}^* \times \underline{B} + \nabla \cdot [2\underline{P} \otimes \underline{E} + \underline{M} \otimes \underline{B} - \frac{1}{2} \underline{P} \cdot \underline{E} \underline{I}] \\ + \underline{i} \times \underline{B} = \rho (\underline{f} - \dot{\underline{v}})$$

and Maxwell's equations are

$$(5.2) \quad \nabla \times \underline{E} + \frac{1}{c} \frac{\partial \underline{B}}{\partial t} = 0, \quad \nabla \times \underline{H} = \frac{1}{c} \frac{\partial \underline{D}}{\partial t} + \frac{4\pi}{c} \underline{J} \\ \nabla \cdot \underline{D} = 4\pi q, \quad \nabla \cdot \underline{B} = 0$$

where for brevity we wrote

$$(5.3) \quad \underline{i} \equiv q_{(e)} \underline{u}^{(es)}, \quad \underline{E} \equiv \underline{E}_{(s)}, \quad \underline{P} \equiv \underline{P}_{(s)}, \quad \underline{M} \equiv \underline{M}_{(s)} \\ \underline{f} \equiv \underline{f}_{(s)}, \quad \rho \equiv \rho_{(s)}, \quad \underline{v} \equiv \underline{v}_{(s)}, \quad q^t = q_{(e)} + q_{(s)} - \nabla \cdot \underline{P}_{(s)}$$

Here, it should be noted that the conduction current \underline{i} is still an unknown, but we have the equations of balance of linear momentum for electrons

$$(5.4) \quad q_{(e)} \underline{E}_{(e)} = \underline{v} \underline{u}_{(es)} - \frac{1}{\chi_1} \underline{E}$$

Recalling the definition of conduction current and (2.8)₁, equation (5.4) may be written as

$$(5.5) \quad \left(\frac{1}{\chi_1} + q_{(e)}\right) \vec{E} + \frac{1}{v} \nabla \times \vec{B} = \frac{v}{q_{(e)}} \vec{i}$$

The solution of \vec{i} from (5.5) is found to be

$$(5.6) \quad i_k = \sigma_{kl} E_l$$

where σ_{kl} is the conductivity tensor given by

$$(5.7) \quad \sigma_{ij} = \frac{\sigma_0}{1 + \frac{B^2 q_e^2}{v^2}} \left[\delta_{ij} + \frac{q_e^2}{v^2} B_i B_j + \frac{q_e}{v} \epsilon_{ijk} B_k \right]$$

with

$$(5.8) \quad \sigma_0 = q_{(e)} (\tau \chi_2^{-1} + q_e) / v$$

In (5.7), the first term on the right-hand side denotes the current parallel to the effective electric field, and the second and third terms give the currents parallel to the magnetic field and perpendicular to the magnetic and electric fields. The last type of current is known as the Hall current. As might be seen from (5.7), the conductivity tensor σ_{kl} is, in general, a function of the magnetic field and the density of electron gas.

Further simplification of (5.7) results, if the following condition holds, i.e.,

$$(5.9) \quad \frac{|B| |q_{(e)}|}{v} \ll 1$$

This condition holds if the gyrofrequency of electrons is small as compared to the collision frequency v . For this case, the conductivity tensor reduces to

$$(5.10) \quad \sigma_{ij} = \sigma_0 \delta_{ij}$$

where σ_0 is called the conductivity constant.

In this case the conduction current becomes

$$(5.11) \quad i_k = \sigma_0 E_k$$

and this is none other than the generalized Ohm's law.

6. SPHERICAL CAVITY SUBJECT TO CONSTANT ELECTROSTATIC POTENTIAL

In this section we give the solution of a problem concerned with a spherical cavity subject to a constant electrostatic potential ϕ_0 and located in an infinite solid plasma. This type of problem, known as electrostatic probe, is widely used in gaseous plasma to determine certain characteristics of probes. It is hoped that the solution of this problem, together with an experiment which can be performed in a manner similar to gaseous probe, will be helpful in determining the material constants appearing in the present derivation. Since the problem is electrostatic in nature, all magnetic and collisional effects are negligible. The field equations (4.13), (4.15), and (4.18)₁, neglecting all the second order terms, reduce to:

$$(6.1) \quad -\nabla^2 \pi_{(e)} + q_{(e)} \underline{E} + \tau P_{(s)} = 0$$

$$(6.2) \quad (\lambda + \mu) \nabla^2 \underline{u} + \mu \nabla^2 \underline{u} + q_{(s)} \underline{E} - \tau P_{(e)} = 0$$

$$(6.3) \quad \nabla \cdot \underline{D} = 4\pi q$$

with

$$(6.4) \quad \underline{D} = \epsilon \underline{E}, \quad q = q_{(s)} + q_{(e)}$$

where ϵ is the dielectric constant defined by

$$\epsilon = 1 + \chi_1^{-1}$$

It is convenient to work with number densities $N_{(a)}$ defined as

$$(6.5) \quad \begin{aligned} \rho_{(e)} &= m_e N_{(e)} \quad , \quad q_{(e)} = -eN_{(e)} \\ \rho_{(s)} &= m_s N_{(s)} \quad , \quad q_{(s)} = ZeN_{(s)} \end{aligned}$$

where m_e , m_s , e and Z are respectively the masses of a particle in electron and solid continua, electronic charge, and the number of valance electrons in the structure of an ionic lattice cell.

In order to proceed further, one must know the forms of $\pi_{(e)}$ and τ . For this particular problem they are assumed to be of the forms

$$(6.6) \quad \pi_{(e)} = K\theta_{(e)}N_{(e)} \quad , \quad \tau = e(Z-\sigma)N_{(s)}$$

where K is the Boltzmann constant, $\theta_{(e)}$ is the electron temperature, and σ is a new constant which characterizes the interaction between the ionic lattice and electronic charge.

Introducing the electrostatic potential ϕ (as usual), and using (6.5) and (6.6) in (6.1) to (6.3), the field equations take the following form

$$(6.7) \quad K\theta_{(e)} \frac{dN_{(e)}}{dr} - eN_{(e)} \frac{d\phi}{dr} + e(Z-\sigma)N_{(s)} \frac{d\phi}{dr} = 0$$

$$(6.8) \quad (\lambda + 2\mu) \frac{d\Delta}{dr} - eZN_{(s)} \frac{d\phi}{dr} + e(Z-\sigma)N_{(s)} \frac{d\phi}{dr} = 0$$

$$(6.9) \quad \nabla^2 \phi = \frac{4\pi e}{\epsilon} (N_{(e)} - ZN_{(s)})$$

where Δ is the volume dilatation defined by

$$\Delta \equiv \frac{1}{r^2} \frac{d}{dr} (r^2 u_r)$$

Recalling the relation

$$N_{(s)} = N_{(s)}^0 (1 - \Delta)$$

The equation (6.8) may be written as

$$(6.10) \quad \frac{(\lambda+2\mu)}{N_{(s)}^0} \frac{dN_{(s)}}{dr} + e\sigma N_{(s)} \frac{d\phi}{dr} = 0$$

where $N_{(s)}^0$ is the undeformed particle number density of the ionic lattice cell.

The equation (6.10) can be integrated to obtain

$$(6.11) \quad N_{(s)} = A \exp\left[-\left(\frac{e\sigma N_{(s)}^0}{\lambda+2\mu}\right)\phi\right]$$

Here A is an integration constant to be determined from the condition

$$(6.12) \quad N_{(s)} \rightarrow N_{(s)}^0, \quad \phi \rightarrow 0, \quad \text{as } r \rightarrow \infty$$

The result is

$$(6.13) \quad N_{(s)} = N_{(s)}^0 \exp\left[-\left(\frac{e\sigma N_{(s)}^0}{\lambda+2\mu}\right)\phi\right]$$

Inserting (6.13) into equation (6.7), and solving the resulting nonhomogeneous differential equation for $N_{(e)}$, we obtain

$$(6.14) \quad N_{(e)} = B \exp\left[\frac{e}{K\theta_{(e)}}\phi\right] + \frac{(Z-\sigma)(\lambda+2\mu)N_{(s)}^0}{(\lambda+2\mu)+K\theta_{(e)}\sigma N_{(s)}^0} \exp\left[-\left(\frac{e\sigma N_{(s)}^0}{\lambda+2\mu}\right)\phi\right]$$

where B is a constant of integration and may be determined from the regularity condition

$$(6.15) \quad N_{(e)} \rightarrow N_{(e)}^0, \quad \phi \rightarrow 0, \quad \text{as } r \rightarrow \infty$$

The use of (6.15) in (6.14) gives the electron number density as

$$(6.16) \quad N_{(e)} = \frac{(z-\sigma)(\lambda+2\mu)N_{(s)}^0}{(\lambda+2\mu)+K\theta_{(e)}N_{(s)}^\sigma} \left\{ \exp\left[-\left(-\frac{e\sigma N_{(s)}^0}{\lambda+2\mu}\right)\phi\right] - \exp\left[\frac{e}{K\theta_{(e)}}\phi\right] + N_{(e)}^c \exp\left[\frac{e}{K\theta_{(e)}}\phi\right] \right\}$$

Here $N_{(e)}^0$ is the initial number density of the electronic charge continuum.

If we introduce (6.13) and (6.16) into (6.9), the resultant ordinary differential equation will be highly nonlinear which cannot be treated by analytical means. This nonlinear equation can be simplified by the following arguments which are similar to the one used in the gaseous plasma, i.e.,

$$(6.17) \quad \left| \frac{e\phi}{K\theta_{(e)}} \right| \ll 1, \quad \left| \frac{e\sigma N_{(s)}^0}{\lambda+2\mu} \phi \right| \ll 1$$

which states that the thermal energy of electronic charge and the elastic energy of the ionic lattice are very large as compared to the electrostatic potential of the medium. This assumption is, in particular, valid at far distances from the surface of the spherical probe. If this is the case, one can expand $N_{(e)}$ and $N_{(s)}$ into a power series of ϕ . Retaining only the first two terms of the series and introducing the result into equation (6.9), we obtain

$$(6.18) \quad \nabla^2 \phi = K_D^2 \phi$$

where K_D^2 is defined by

$$K_D^2 = \frac{4\pi e^2}{\epsilon} \left[\left(\frac{1}{K\theta_{(e)}} + \frac{Z\sigma N_{(s)}^0}{\lambda+2\mu} \right) \left(1 - \frac{(Z-\sigma)(\lambda+2\mu)N_{(s)}^0}{(\lambda+2\mu)+K\theta_{(e)}\sigma N_{(s)}^0} \right) \right]$$

In obtaining the equation (6.18), we have required the charge neutrality at the initial state, i.e.,

$$(6.19) \quad N_{(e)}^0 = ZN_{(s)}^0$$

In addition, we require that $K_D^2 \geq 0$. This condition is known as the Bohm shielding criteria.

The solution of (6.18), with vanishing ϕ at infinity, is given by

$$(6.20) \quad \phi = C \frac{e^{-K_D r}}{r}$$

Here C is a constant of integration which may be determined by equating the potential to the given potential ϕ_0 at the surface of the probe.

The result is:

$$(6.21) \quad \phi = \phi_0 e^{-K_D(r-a)} \left(\frac{a}{r} \right)$$

where a is the radius of the metallic probe.

From the definition of dilatation and its relation to the number density of a solid continuum, one can find the radial component of displacement satisfying the stress free boundary condition. The final result is given by

$$(6.22) \quad u_r = \left[\frac{a^3}{4\mu} + \frac{1}{\lambda+2\mu} \left(\frac{a^2}{K_D} + \frac{a}{K_D^2} \right) \right] \frac{e\sigma\phi_0}{r^2} - \frac{e\sigma\phi_0 a}{\lambda+2\mu} \left(\frac{1}{K_D r} + \frac{1}{K_D^2 r^2} \right) e^{-K_D(r-a)}$$

$$u_\theta = u_\phi = 0$$

Similarly, the approximate number densities are:

$$\begin{aligned}
 (6.23) \quad N_{(s)} &\approx N_{(s)}^0 \left[1 - \frac{e\sigma\phi_0 a}{\lambda+2\mu} \frac{e^{-K_D(r-a)}}{r} \right] \\
 N_{(e)} &\approx N_{(e)}^0 \left[1 + S a \phi_0 \frac{e^{-K_D(r-a)}}{r} \right]
 \end{aligned}$$

where S is defined as

$$S \equiv \frac{e}{K\theta_{(e)}} - e \left(\frac{\sigma}{Z(\lambda+2\mu)} + \frac{1}{K\theta_{(e)}} \right) \left(\frac{(Z-\sigma)(\lambda+2\mu)}{(\lambda+2\mu)Z + K\theta_{(e)} N_{(e)}^0 \sigma} \right)$$

From these equations one can evaluate the values of displacement and the number of densities on the surface of the sphere. These are:

$$\begin{aligned}
 (6.24) \quad u_r(a) &= \frac{e\sigma\phi_0 a}{4\mu}, \quad N_{(s)}(a) = N_{(s)}^0 \left(1 - \frac{e\sigma\phi_0}{\lambda+2\mu} \right) \\
 N_{(e)}(a) &= N_{(e)}^0 (1 + S a \phi_0)
 \end{aligned}$$

From physical considerations, one expects that

$$\frac{\sigma}{\lambda+2\mu} \geq 0, \quad S \geq 0$$

This requirement is consistent with the one posed for K_D^2 .

If the same problem was solved by use of the classical theory of elastic conductors, the result would be

$$(6.25) \quad \phi = \phi_0 \left(\frac{a}{r} \right)$$

which is equivalent to equation (6.21) as K_D^2 approaches to zero.

As a concluding remark, it is worthwhile to cite that the present approach not only gives the distribution of electrostatic potential but also the variations of the densities of the electronic and ionic species that form an elastic conductor.

REFERENCES

1. R. A. Grot and A. C. Eringen, Int. J. Engng. Sci., 4, 611 (1966).
2. N. F. Jordan and A. C. Eringen, Int. J. Engng. Sci., 2, 59 (1964).
3. J. B. Walker, Int. J. Nonlinear Mech., 2, 245 (1967).
4. H. Demiray and A. C. Eringen, "Continuum Theory of Slightly Ionized Plasmas - Diamagnetic Effects", (Submitted for Publication)
5. R. C. Dixon and A. C. Eringen, Int. J. Engng. Sci., 3, 359 (1965).
6. R. A. Toupin, Int. J. Engng. Sci., 1, 101 (1963).

PART 1 - GOVERNMENT

Administrative & Liaison Activities

Chief of Naval Research
Department of the Navy
Washington, D. C. 20360
Attn: Code 423

439
468

Director
CNR Branch Office
495 Summer Street
Boston, Massachusetts 02210

Director
ONR Branch Office
219 S. Dearborn Street
Chicago, Illinois 60604

Dir., Naval Res. Lab.
Attn: Library, Code 2029 (ONRL)
Washington, D. C. 20390

Commanding Officer
ONR Branch Office
207 West 24th Street
New York, New York 10011

Director
ONR Branch Office
1030 E. Green Street
Pasadena, California 91101

U. S. Naval Research Laboratory
Attn: Technical Information Div.
Washington, D. C. 20390

Defense Documentation Center
Cameron Station
Alexandria, Virginia 22314

Army

Commanding Officer
U. S. Army Research Off. Durham
Attn: Mr. J. J. Murray
CRD-AA-IP
Box CM, Duke Station
Durham, North Carolina 27706

Commanding Officer
AMXMR-ATL
Attn: Mr. J. Bluhm
U. S. Army Materials Res. Agcy.
Watertown, Massachusetts 02172

(2) Watervliet Arsenal
MAGGS Research Center
Watervliet, New York
Attn: Director of Research

Redstone Scientific Info. Center
Chief, Document Section
U. S. Army Missile Command
Redstone Arsenal, Alabama 35809

Army R & D Center
Fort Belvoir, Virginia 22060

Technical Library
Aberdeen Proving Ground
Aberdeen, Maryland 21005

(5)

Navy

Commanding Officer and Director
Naval Ship Research & Development Center
Washington, D. C. 20007

Attn: Code 042 (Tech. Lib. Br.)
700 (Struc. Mech. Lab.)
720
725
800 (Appl. Math. Lab.)
012.2 (Mr. W. J. Sette)
901 (Dr. M. Strassberg)
941 (Dr. R. Liebowitz)
945 (Dr. W. S. Cramer)
960 (Mr. E. F. Noonan)
962 (Dr. E. Buchmann)

Aeronautical Structures Lab.
Naval Air Engineering Center
Naval Base, Philadelphia, Pa. 19112

Naval Weapons Laboratory
Dahlgren, Virginia 22448

Naval Research Laboratory
Washington, D. C. 20390
Attn: Code 8400
8430
8440

Office of Naval Research
Resident Representative
Theobald Smith House-Forrestal Campus
Princeton University
Princeton, New Jersey 08540

Undersea Explosion Research Div.
Naval Ship R & D Center
Norfolk Naval Shipyard
Portsmouth, Virginia 23709
Attn: Mr. D. S. Cohen
Code 780

Nav. Ship R & D Center
Annapolis Division
Code 257, Library
Annapolis, Maryland 21402

Technical Library
Naval Underwater Weapons Center
Pasadena Annex
3202 E. Foothill Blvd.
Pasadena, California 91107

U. S. Naval Weapons Center
China Lake, California 93557
Attn: Code 4062 Mr. W. Werback
4520 Mr. Ken Bischel

Naval Research Laboratory
Washington, D. C. 20390
Attn: Code 8400 Ocean Tech. Div.
8440 Ocean Structures
6300 Metallurgy Div.
6305 Dr. J. Krafft

Commanding Officer
U. S. Naval Civil Engr. Lab.
Code L31
Port Hueneme, California 93041

Shipyard Technical Library
Code 242 L
Portsmouth Naval Shipyard
Portsmouth, New Hampshire 03804

U. S. Naval Electronics Laboratory
Attn: Dr. R. J. Christensen
San Diego, California 92152

U. S. Naval Ordnance Laboratory
Mechanics Division
RFD 1, White Oak
Silver Spring, Maryland 20910

U. S. Naval Ordnance Laboratory
Attn: Mr. H. A. Perry, Jr.
Non-Metallic Materials Division
Silver Spring, Maryland 20910

Supervisor of Shipbuilding
U. S. Navy
Newport News, Virginia 23607

Shipyard Technical Library
Building 746, Code 303TL
Mare Island Naval Shipyard
Vallejo, California 94592

U. S. Navy Underwater Sound Ref. Lab.
Office of Naval Research
P. O. Box 8337
Orlando, Florida 32806

Technical Library
U. S. Naval Ordnance Station
Indian Head, Maryland 20640

U. S. Naval Ordnance Station
Attn: Mr. Garet Bornstein
Research & Development Division
Indian Head, Maryland 20640

Chief of Naval Operation
Department of the Navy
Washington, D. C. 20350
Attn: Code Op-03EG
Op-07T

Special Projects Office
(CNM-PM-1) (MUN)
Department of the Navy
Washington, D. C. 20360
Attn: NSP-001 Dr. J. P. Craven

Deep Submergence Sys. Project
(CNM-PM-11)
6900 Wisconsin Avenue
Chevy Chase, Md. 20015
Attn: PM-1120 S. Hersh

Director Aeronautical Materials Lab.
Naval Air Engineering Center
Naval Base
Philadelphia, Pennsylvania 19112

Naval Air Systems Command
Dept. of the Navy
Washington, D. C. 20360
Attn: NAIR 03 Res. & Technology
320 Aero. & Structures
5320 Structures
604 Tech. Library

Naval Facilities Engineering
Command
Dept. of the Navy
Washington, D. C. 20360
Attn: NFAC 03 Res. & Development
04 Engineering & Design
04128 Tech. Library

Naval Ship Systems Command
Dept. of the Navy
Washington, D. C. 20360
Attn: NSHIP 031 Ch. Scientists for R & D
0342 Ship Mats. & Structs.
037 Ship Silencing Div.
052 Shock & Blast Coord.
2052 Tech. Library

Naval Ship Engineering Center
Main Navy Building
Washington, D. C. 20360
Attn: NSEC 6100 Ship Sys. Engr. & Des. Dept.
6102C Computerized Ship Des.
6105 Ship Protection
6110 Ship Concept Design
6120 Hull Div. - J. Nachtsheim
6120D Hull Div. - J. Vasta
6132 Hull Structs. - (4)

Naval Ordnance Systems Command
Dept. of the Navy
Washington, D. C. 20360
Attn: NORD 03 Res. & Technology
035 Weapons Dynamics
9132 Tech. Library

Air Force

Commander WADD
Wright-Patterson Air Force Base
Dayton, Ohio 45433
Attn: Code WWRMDD
AFFDL (FDDS)

Wright-Patterson AFB (cont'd)
Attn: Structures Division
AFLC (MCEFA)
Code WWRC
AFML (MAAM)
Code WCLSY
SEG (SEFSD, Mr. Lakin)

Commander
Chief, Applied Mechanics Group
U. S. Air Force Inst. of Tech.
Wright-Patterson Air Force Base
Dayton, Ohio 45433

Chief, Civil Engineering Branch
WLRC, Research Division
Air Force Weapons Laboratory
Kirtland AFB, New Mexico 87117

Air Force Office of Scientific Res.
1400 Wilson Blvd.
Arlington, Virginia 22209
Attn: Mechs. Div.

NASA

Structures Research Division
National Aeronautics & Space Admin.
Langley Research Center
Langley Station
Hampton, Virginia 23365
Attn: Mr. R. R. Heldenfels, Chief

National Aeronautic & Space Admin.
Associate Administrator for Advanced
Research & Technology
Washington, D. C. 20546

Scientific & Tech. Info. Facility
NASA Representative (S-AK/DL)
P.O. Box 5700
Bethesda, Maryland 20014

National Aeronautic & Space Admin.
Code RV-2
Washington, D. C. 20546

Other Government Activities

Commandant

Chief, Testing & Development Div.
U. S. Coast Guard
1300 E Street, N. W.
Washington, D. C. 20226

Director

Marine Corps Landing Force Devel. Cen.
Marine Corps Schools
Quantico, Virginia 22134

Director

National Bureau of Standards
Washington, D. C. 20234
Attn: Mr. B. L. Wilson, EM 219

National Science Foundation
Engineering Division
Washington, D. C. 20550

Science & Tech. Division
Library of Congress
Washington, D. C. 20540

Director

STBS
Defense Atomic Support Agency
Washington, D. C. 20350

Commander Field Command
Defense Atomic Support Agency
Sandia Base
Albuquerque, New Mexico 87115

Chief, Defense Atomic Support Agcy.
Blast & Shock Division.
The Pentagon
Washington, D. C. 20301

Director Defence Research & Engr.
Technical Library
Room 3C-128
The Pentagon
Washington, D. C. 20361

Chief, Airframe & Equipment Branch
FS-120
Office of Flight Standards
Federal Aviation Agency
Washington, D. C. 20553

Chief, Division of Ship Design
Maritime Administration
Washington, D. C. 20235

Deputy Chief, Office of Ship Constr.
Maritime Administration
Washington, D. C. 20235
Attn: Mr. U. L. Russo

Mr. Milton Shaw, Director
Div. of Reactor Devel. & Technology
Atomic Energy Commission
Germantown, Md. 20767

Ship Hull Research Committee
National Research Council
National Academy of Sciences
2101 Constitution Avenue
Washington, D. C. 20418
Attn: Mr. A. R. Lytle

PART 2 - CONTRACTORS AND OTHER TECHNICAL COLLABORATORS

Universities

Professor J. R. Rice
Division of Engineering
Brown University
Providence, Rhode Island 02912

Dr. J. Tinsley Oden
Dept. of Engr. Mechs.
University of Alabama
Huntsville, Alabama

Professor M. E. Gurtin
Dept. of Mathematics
Carnegie Institute of Technology
Pittsburgh, Pennsylvania 15213

Professor R. S. Rivlin
Center for the Application of Mathematics
Lehigh University
Bethlehem, Pennsylvania 18015

Professor Julius Miklowitz
Division of Engr. & Applied Sciences
California Institute of Technology

Professor George Sih
Department of Mechanics
Lehigh University
Bethlehem, Pennsylvania 18015

Dr. Harold Liebowitz, Dean
School of Engr. & Applied Science
George Washington University
725 23rd Street
Washington, D. C. 20006

Professor Eli Sternberg
Div. of Engr. & Applied Sciences
California Institute of Technology
Pasadena, California 91109

Professor Paul M. Naghdi
Div. of Applied Mechanics
Etcheverry Hall
University of California
Berkeley, California 94720

Professor Wm. Prager
Revelle College
University of California
P. O. Box 109
La Jolla, California 92037

Professor J. Baltrukonis
Mechanics Division
The Catholic University of America
Washington, D. C. 20017

Professor A. J. Durelli
Mechanics Division
The Catholic University of America
Washington, D. C. 20017

Professor H. H. Bleich
Department of Civil Engr.
Columbia University
S. W. Mudd Building
New York, New York 10027

Professor F. L. DiMaggio
Department of Civil Engr.
Columbia University
616 Mudd Building
New York, New York 10027

Professor A. M. Freudenthal
Department of Civil Engr. &
Engr. Mech.
Columbia University
New York, New York 10027

Professor B. A. Boley
Department of Theor. & Appl. Mech.
Cornell University
Ithaca, New York 14850

Professor P. G. Hodge
Department of Mechanics
Illinois Institute of Technology
Chicago, Illinois 60616

Dr. D. C. Drucker
Dean of Engineering
University of Illinois
Urbana, Illinois 61803

Professor N. M. Newmark
Dept. of Civil Engineering
University of Illinois
Urbana, Illinois 61803

Professor A. R. Robinson
Department of Civil Engr.
University of Illinois
Urbana, Illinois 61803

Professor S. Taira
Department of Engineering
Kyoto University
Kyoto, Japan

Professor James Mar
Massachusetts Inst. of Tech.
Rm. 33-318
Dept. of Aerospace & Astro.
77 Massachusetts Avenue
Cambridge, Mass. 02139

Professor E. Reissner
Dept. of Mathematics
Massachusetts Inst. of Tech.
Cambridge, Mass. 02139

Professor William A. Nash
Dept. of Mechs. & Aerospace Engr.
University of Mass.
Amherst, Mass. 01002

Library (Code 0384)
U. S. Naval Postgraduate School
Monterey, California 93940

Professor Arnold Allentuch
Dept. of Mechanical Engineering
Newark College of Engineering
323 High Street
Newark, New Jersey 07102

Professor R. D. Mindlin
Department of Civil Engr.
Columbia University
S. W. Mudd Building
New York, New York 10027

Professor E. L. Reiss
Courant Inst. of Math. Sciences
New York University
4 Washington Place
New York, New York 10003

Professor Bernard W. Shaffer
School of Engrg. & Science
New York University
University Heights
New York, New York 10453

Dr. Francis Cozzarelli
Div. of Interdisciplinary
Studies and Research
School of Engineering
State Univ. of New York
Buffalo, New York 14214

Professor R. A. Douglas
Dept. of Engr. Mechs.
North Carolina State Univ.
Raleigh, North Carolina 27607

Dr. George Herrmann
The Technological Institute
Northwestern University
Evanston, Illinois 60201

Professor J. D. Achenbach
Technological Institute
Northwestern University
Evanston, Illinois 60201

Director, Ordnance Research Lab.
Pennsylvania State University
P. O. Box 30
State College, Pennsylvania 16801

Professor Eugene J. Skudrzyk
Department of Physics
Ordnance Research Lab.
Pennsylvania State University
P. O. Box 30
State College, Pennsylvania 16801

Dean Oscar Baguio
Assoc. of Struc. Engr. of the Philippines
University of Philippines
Manila, Philippines

Professor J. Kempner
Dept. of Aero. Engr. & Appl. Mech.
Polytechnic Institute of Brooklyn
333 Jay Street
Brooklyn, New York 11201

Professor J. Klosner
Polytechnic Institute of Brooklyn
333 Jay Street
Brooklyn, New York 11201

Professor A. C. Eringen
Dept. of Aerospace & Mech. Sciences
Princeton University
Princeton, New Jersey 08540

Dr. S. L. Koh
School of Aero., Astro. & Engr. Sci.
Purdue University
Lafayette, Indiana 47907

Professor R. A. Schapery
Purdue University
Lafayette, Indiana 47907

Professor E. H. Lee
Div. of Engr. Mechanics
Stanford University
Stanford, California 94305

Dr. Nicholas J. Hoff
Dept. of Aero. & Astro.
Stanford University
Stanford, California 94305

Professor Max Anliker
Dept. of Aero. & Astro.
Stanford University
Stanford, California 94305

Professor J. N. Goodier
Div. of Engr. Mechanics
Stanford University
Stanford, California 94305

Professor H. W. Liu
Dept. of Chemical Engr. & Metal.
Syracuse University
Syracuse, New York 13210

Professor Markus Reiner
Technion R & D Foundation
Haifa, Israel

Professor Tsuyoshi Hayashi
Department of Aeronautics
Faculty of Engineering
University of Tokyo
Bunkyo-Ku
Tokyo, Japan

Professor J. E. Fitzgerald, Ch.
Dept. of Civil Engineering
University of Utah
Salt Lake City, Utah 84112

Professor R. J. H. Bollard
Chairman, Aeronautical Engr. Dept.
207 Guggenheim Hall
University of Washington
Seattle, Washington 98105

Professor Albert S. Kobayashi
Dept. of Mechanical Engr.
University of Washington
Seattle, Washington 98105

Officer-in-Charge
Post Graduate School for Naval Off.
Webb Institute of Naval Arch.
Crescent Beach Road, Glen Cove
Long Island, New York 11542

Librarian
Webb Institute of Naval Arch.
Crescent Beach Road, Glen Cove
Long Island, New York 11542

Solid Rocket Struc. Integrity Cen.
Dept. of Mechanical Engr.
Professor F. Wagner
University of Utah
Salt Lake City, Utah 84112

Dr. Daniel Frederick
Dept. of Engr. Mech.
Virginia Polytechnic Inst.
Blacksburgh, Virginia

Industry and Research Institutes

Dr. James H. Wiegand
Senior Dept. 4720, Bldg. 0525
Ballistics & Mech. Properties Lab.
Aerojet-General Corporation
P. O. Box 1947
Sacramento, California 95809

Mr. Carl E. Hartbower
Dept. 4620, Bldg. 2019 A2
Aerojet-General Corporation
P. O. Box 1947
Sacramento, California 95809

Mr. J. S. Wise
Aerospace Corporation
P. O. Box 1300
San Bernardino, California 92402

Dr. Vito Salerno
Applied Technology Assoc., Inc.
29 Church Street
Ramsey, New Jersey 07446

Library Services Department
Report Section, Bldg. 14-14
Argonne National Laboratory
9700 S. Cass Avenue
Argonne, Illinois 60440

Dr. M. C. Junger
Cambridge Acoustical Associates
129 Mount Auburn Street
Cambridge, Massachusetts 02138

Dr. F. R. Schwarzl
Central Laboratory T.N.O.
Schoemakerstraat 97
Delft, The Netherlands

Research and Development
Electric Boat Division
General Dynamics Corporation
Groton, Connecticut 06340

Supervisor of Shipbuilding, USN,
and Naval Insp. of Ordnance
Electric Boat Division
General Dynamics Corporation
Groton, Connecticut 06340

Dr. L. H. Chen
Basic Engineering
Electric Boat Division
General Dynamics Corporation
Groton, Connecticut 06340

Dr. Wendt
Valley Forge Space Technology Cen.
General Electric Co.
Valley Forge, Pennsylvania 10481

Dr. Joshua E. Greenspon
J. G. Engr. Research Associates
3831 Menlo Drive
Baltimore, Maryland 21215

Dr. Walt D. Pilkey
IIT Research Institute
10 West 35 Street
Chicago, Illinois 60616

Library Newport News Shipbuilding
& Dry Dock Company
Newport News, Virginia 23607

Mr. J. I. Gonzalez
Engr. Mechs. Lab.
Martin Marietta
MP - 233
P. O. Box 5837
Orlando, Florida 32805

Dr. E. A. Alexander
Research Dept.
Rocketdyne D. W., NAA
6633 Canoga Avenue
Canoga Park, California 91304

Mr. Cezar P. Nuguid
Deputy Commissioner
Philippine Atomic Energy
Commission
Manila, Philippines

Dr. M. L. Merritt
Division 5412
Sandia Corporation
Sandia Base
Albuquerque, New Mexico 87115

Director
Ship Research Institute
Ministry of Transportation
700, Shinkawa
Mitaka
Tokyo, Japan

Dr. H. N. Abramson
Southwest Research Institute
8500 Culebra Road
San Antonio, Texas 78206

Dr. R. C. DeHart
Southwest Research Institute
8500 Culebra Road
San Antonio, Texas 78206

Dr. M. L. Baron
Paul Weidlinger, Consulting Engr.
777 Third Ave. - 22nd Floor
New York, New York 10017

Mr. Roger Weiss
High Temp. Structs. & Materials
Applied Physics Lab.
8621 Georgia Avenue
Silver Spring, Md.

Mr. William Caywood
Code BBE
Applied Physics Lab.
8621 Georgia Avenue
Silver Spring, Md.

Mr. M. J. Berg
Engineering Mechs. Lab.
Bldg. R-1, Rm. 1104A
TRW Systems
1 Space Park
Redondo Beach, California 90278

Professor Tsuyoshi Hayashi
Department of Aeronautics
Faculty of Engineering
University of Tokyo
Bunkyo-Ku
Tokyo, Japan

Professor J. E. Fitzgerald, Ch.
Dept. of Civil Engineering
University of Utah
Salt Lake City, Utah 84112

Professor R. J. H. Bollard
Chairman, Aeronautical Engr. Dept.
207 Guggenheim Hall
University of Washington
Seattle, Washington 98105

Professor Albert S. Kobayashi
Dept. of Mechanical Engr.
University of Washington
Seattle, Washington 98105

Officer-in-Charge
Post Graduate School for Naval Off.
Webb Institute of Naval Arch.
Crescent Beach Road, Glen Cove
Long Island, New York 11542

Librarian
Webb Institute of Naval Arch.
Crescent Beach Road, Glen Cove
Long Island, New York 11542

Solid Rocket Struc. Integrity Cen.
Dept. of Mechanical Engr.
Professor F. Wagner
University of Utah
Salt Lake City, Utah 84112

Dr. Daniel Frederick
Dept. of Engr. Mechs.
Virginia Polytechnic Inst.
Blacksburgh, Virginia

Industry and Research Institutes

Dr. James H. Wiegand
Senior Dept. 4720, Bldg. 0525
Ballistics & Mech. Properties Lab.
Aerojet-General Corporation
P. O. Box 1947
Sacramento, California 95809

Mr. Carl E. Hartbower
Dept. 4620, Bldg. 2019 A2
Aerojet-General Corporation
P. O. Box 1947
Sacramento, California 95809

Mr. J. S. Wise
Aerospace Corporation
P. O. Box 1300
San Bernardino, California 92402

Dr. Vito Salerno
Applied Technology Assoc., Inc.
29 Church Street
Ramsey, New Jersey 07446

Library Services Department
Report Section, Bldg. 14-14
Argonne National Laboratory
9700 S. Cass Avenue
Argonne, Illinois 60440

Dr. M. C. Junger
Cambridge Acoustical Associates
129 Mount Auburn Street
Cambridge, Massachusetts 02138

Dr. F. R. Schwarzl
Central Laboratory T.N.O.
Schoenmakerstraat 97
Delft, The Netherlands

Research and Development
Electric Boat Division
General Dynamics Corporation
Groton, Connecticut 06340

Supervisor of Shipbuilding, USN,
and Naval Insp. of Ordnance
Electric Boat Division
General Dynamics Corporation
Groton, Connecticut 06340

Dr. L. H. Chen
Basic Engineering
Electric Boat Division
General Dynamics Corporation
Groton, Connecticut 06340

Dr. Wendt
Valley Forge Space Technology Cen.
General Electric Co.
Valley Forge, Pennsylvania 10481

Dr. Joshua E. Greenspon
J. G. Engr. Research Associates
3831 Menlo Drive
Baltimore, Maryland 21215

Dr. Walt D. Pilkey
IIT Research Institute
10 West 35 Street
Chicago, Illinois 60616

Library Newport News Shipbuilding
& Dry Dock Company
Newport News, Virginia 23607

Mr. J. I. Gonzalez
Engr. Mechs. Lab.
Martin Marietta
MP - 233
P. O. Box 5837
Orlando, Florida 32805

Dr. E. A. Alexander
Research Dept.
Rocketdyne D. W., NAA
6633 Canoga Avenue
Canoga Park, California 91304

Mr. Cezar F. Nuguid
Deputy Commissioner
Philippine Atomic Energy
Commission
Manila, Philippines

Dr. M. L. Merritt
Division 5412
Sandia Corporation
Sandia Base
Albuquerque, New Mexico 87115

Director
Ship Research Institute
Ministry of Transportation
700, Shinkawa
Mitaka
Tokyo, Japan

Dr. H. N. Abramson
Southwest Research Institute
8500 Culebra Road
San Antonio, Texas 78206

Dr. R. C. Dellart
Southwest Research Institute
8500 Culebra Road
San Antonio, Texas 78206

Dr. M. L. Baron
Paul Weidlinger, Consulting Engr.
777 Third Ave. - 22nd Floor
New York, New York 10017

Mr. Roger Weiss
High Temp. Structs. & Materials
Applied Physics Lab.
8621 Georgia Avenue
Silver Spring, Md.

Mr. William Caywood
Code BBE
Applied Physics Lab.
5621 Georgia Avenue
Silver Spring, Md.

Mr. M. J. Berg
Engineering Mechs. Lab.
Bldg. R-1, Rm. 1104A
TRW Systems
1 Space Park
Redondo Beach, California 90278